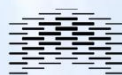


## Operative temperature in the sun

Line Røseth Karlsen<sup>\*,\*\*</sup>, Per Heiselberg<sup>\*\*</sup>, Ida Bryn<sup>\*</sup>

<sup>\*</sup>Oslo and Akershus University College

<sup>\*\*</sup>Aalborg University



OSLO AND AKERSHUS  
UNIVERSITY COLLEGE  
OF APPLIED SCIENCES



AALBORG UNIVERSITY  
DENMARK

## Why is this important?

- Radiative heat exchange significantly affect the thermal sensation experienced by a person in a confined environment.
- In todays commercial buildings with large portions of glazing in the facade, solar radiation might play an important role in the indoor environment.

## How is thermal comfort in the sun treated in building simulation tools?

### SIMIEN

- Isothermal surface temperature.
  - Radiation heat gain is assumed to be distributed evenly on the different opaque surfaces in the room.
  - Direct sun on the human is not accounted for.

### IDA ICE 4.5

- Mean radiant temperature is calculated based on view factors between the zone and an infinitely small cube.
  - Direct sun radiation through window before first reflection is not accounted for.
  - Do not take into account the contribution of solar radiation on the human body.

## Case study

Office building Bjørvika Oslo 59N10E

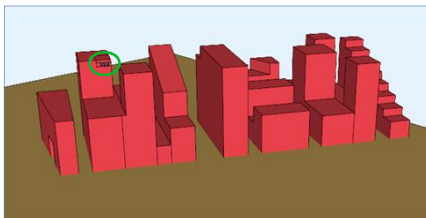


Figure 1: Sketchup model of the office building in its surrounding environment

Model of the team-office which is object for the case study



Figure 2: Model of the team-office. Solar shading is not in use.

# Case study

## IDA ICE model

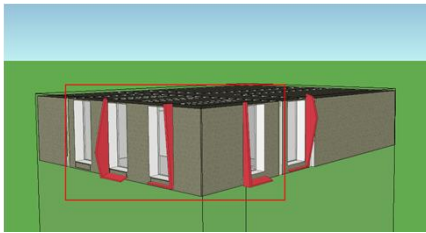


Figure 3: Simulation model for IDA ICE

## Building properties

U-value wall	0.17 W/m <sup>2</sup> K
U-value roof	0.12 W/m <sup>2</sup> K
Normalised thermal bridge	0.06 W/K m <sup>2</sup> floor area
U-value window	1.1 W/m <sup>2</sup> K
g-value window	0.27
τ, solar transmittance	0.24
VAV-ventilation	2-3 l/s / 0.6 l/s
Active beam cooling	60 W/m <sup>2</sup>
Set point heating (NS3031)	21/19
Set point cooling (NS3031)	22
Internal gains (NS3031)	light 8 W/m <sup>2</sup> Equipment 11 W/m <sup>2</sup> People 4 W/m <sup>2</sup>

# Case study

## No solar shading

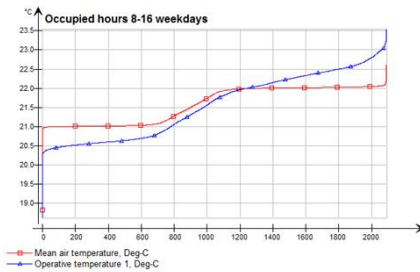


Figure 4: Duration mean air temperature and operative teperature in position 1, no solar shading, weather data NS3031

Total energy demand: 135 kWh/m<sup>2</sup>

## Comparison no solar shading – internal blinds

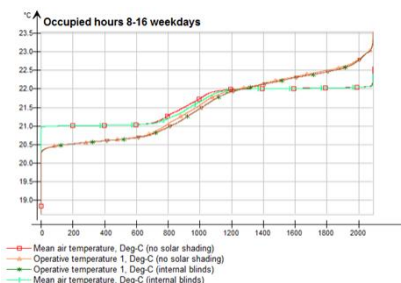


Figure 5: Comparison duration mean air temperature and operative teperature in position 1, no solar shading vs. Internal blinds, weather data NS3031

Total energy demand: 136 kWh/m<sup>2</sup>

## Calculation of operative temperature in the sun

Mean radiant temperature of an object exposed to directional irradiation from a high-intensity radiant source according to P.O. Fanger:

$$T_{mrt} = \sqrt[4]{(T_{umrt}^4 + (\text{const} \cdot f_p \cdot \alpha_{ir} \cdot q_{ir}))}$$

$T_{mrt}$	: mean radiant temperature of irradiated person
$T_{umrt}$	: mean radiant temperature of unirradiated person
const	: $\frac{1}{\epsilon_p \cdot \sigma}$
$\epsilon_p$	: emittance (0,97)
$\sigma$	: Stephan Boltzmanns constant
$f_p$	: projected area factor (0.25 for the sphere)
$\alpha_{ir}$	: absobtance of outer surface of the object (assumed to be 0.85 for this case)
$q_{ir}$	: irradiation from the source

## Calculation of operative temperature in the sun

$$q_{ir} = (I_{bn} \cdot \cos\theta + \frac{3}{4}I_{dh} + \frac{\rho}{4}(I_{bh} + I_{dh})) \cdot \tau$$

$q_{ir}$	: solar radiation
$I_{bn}$	: beam normal radiation
$I_{dh}$	: diffuse horizontal radiation
$I_{bh}$	: beam horizontal radiation
$\theta$	: angle of incidence
$\rho$	: outdoor reflectance (assumed 0,2 for this case)
$\tau$	: direct solar transmittance of window (0,24 in this case)

- Ida Bryn and Marit Smitsrød tried to test this model in 2001
  - restricted data with sunny weather
  - promising results.

# Case study

## IDA ICE model

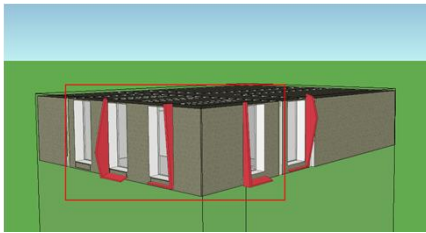


Figure 6: Simulation model for IDA ICE

## Building properties

U-value wall	0.17 W/m <sup>2</sup> K
U-value roof	0.12 W/m <sup>2</sup> K
Normalised thermal bridge	0.06 W/K m <sup>2</sup> floor area
U-value window	1.1 W/m <sup>2</sup> K
g-value window	0.27
τ, solar transmittance	0.24
VAV-ventilation	2-3.5 l/s / 0.8 l/s
Active beam cooling	60 W/m <sup>2</sup>
Set point heating	20.3
Set point cooling	21.5
light	12 W/m <sup>2</sup>
Internal gains Equipment	9 W/m <sup>2</sup>
Internal gains People	6 W/m <sup>2</sup>

# Experimental setup

## Measurement points

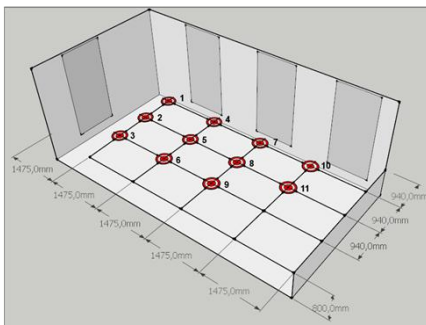
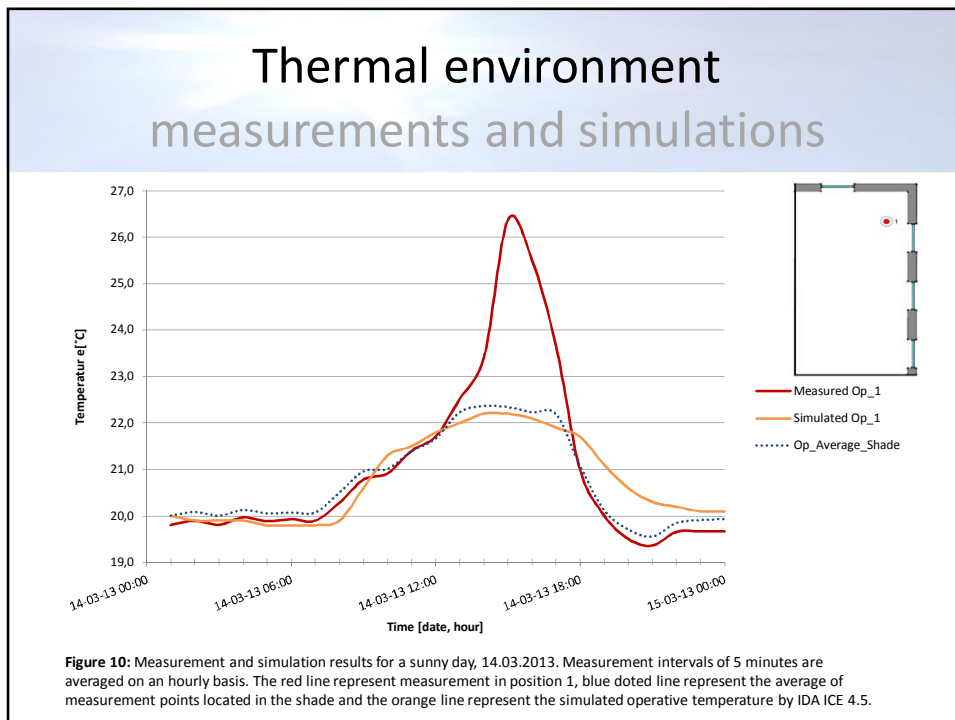
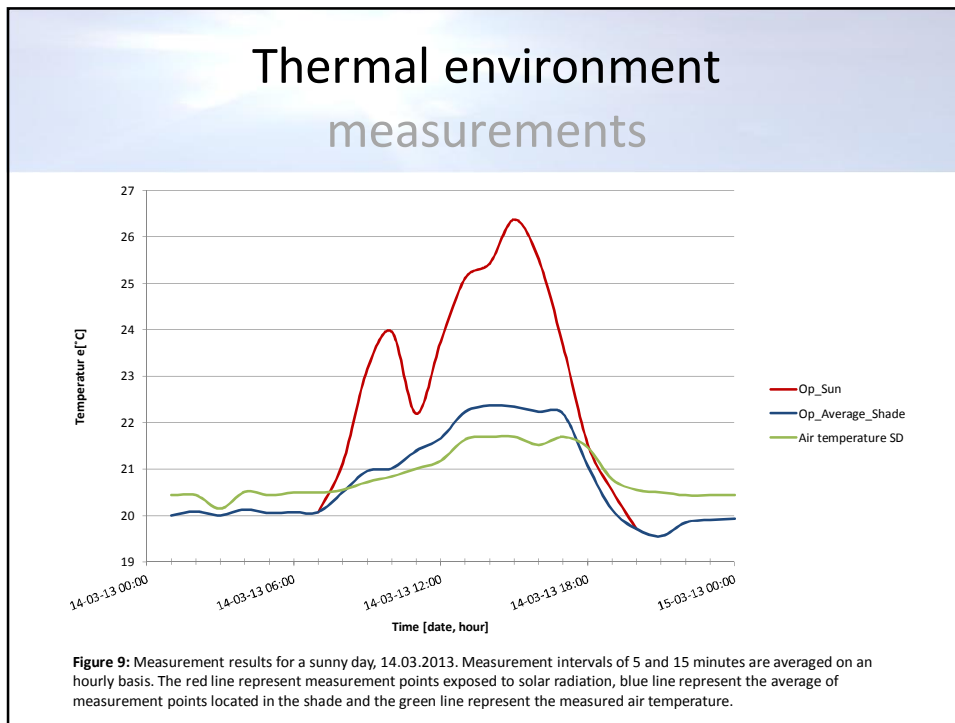


Figure 7: Illustration of location of measurement points.

## Instrumental setup



Figure 8: Photo of instrumental setup, illuminance meter (0,85 m) globe thermometer (1,1 m). Photo: Silje Bjørkeng



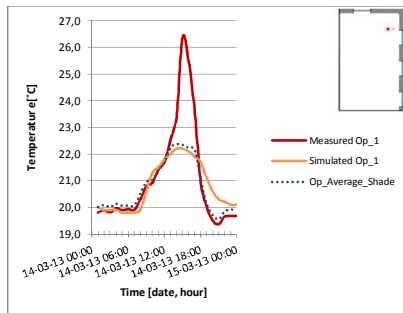
# Operative temperature in the sun calculations

**Table 1:** Calculation of operative temperature for sunny conditions during the experiment period

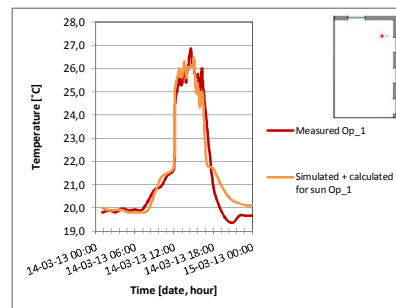
Time	Weather conditions	Measured air temperature [°C]	Measured operative temperature in shadow [°C]	Diffuse horizontal radiation (calculated based on Skartveit og Olsenh 1998) [W/m²]	Direct normal radiation (calculated based on Skartveit og Olsenh 1998) [W/m²]	calculated solar radiation [W/m²]	Calculated radiant temperature T <sub>umrt</sub> [°C]	calculated mean radiant temperature, T <sub>mrt</sub> [°C]	calculated operative temperature in the sun [°C]	measured operative temperature in the sun [°C]	Relative error in percentage with respect to measured values [%]	Comment
12.03.2013 15:00	sunny	21,7	22,2	85	627	738,4	22,7	29,0	25,4	25,9	2,074	
12.03.2013 16:00		21,7	21,9	129	707	656,8	22,2	27,8	24,7	25,1	1,447	
12.03.2013 17:00		21,8	22,1	93	638	504,6	22,5	26,8	24,3	23,9	-1,021	Not sun the whole hour
13.03.2013 15:00	sunny	22,0	22,4	110	839	870,2	22,7	30,1	26,1	26,4	1,265	
13.03.2013 16:00		21,8	22,1	124	741	790,3	22,3	29,1	25,4	26,0	2,196	
13.03.2013 17:00		21,8	21,8	100	654	640,5	21,9	27,5	24,6	23,9	-2,922	Not sun the whole hour
14.03.2013 14:00	sunny	21,9	22,1	102,8	875,1	865,3	22,3	29,7	25,8	25,6	-0,631	
14.03.2013 15:00		22,0	22,4	121,7	825,5	876,0	22,8	30,2	26,1	26,9	0,966	
14.03.2013 16:00		21,7	22,0	125,6	748,4	796,1	22,4	29,2	25,4	25,6	0,073	
18.03.2013 12:00	Partly cloudy	21,5	21,9	137	625	499,4	22,3	26,6	24,0	23,6	-1,865	Not sun the whole hour
18.03.2013 13:00		21,8	22,0	135	779	715,9	22,2	28,4	25,1	23,9	-4,871	Not sun the whole hour
18.03.2013 14:00		22,2	22,2	119	414	589,9	22,3	26,7	24,5	25,9	3,230	Not sun the whole hour
18.03.2013 15:00		22,0	22,1	118	614	666,8	22,3	28,0	25,0	25,7	2,710	
18.03.2013 16:00		21,4	21,6	120	211	288,7	21,8	24,3	22,9	24,4	6,407	Weather data from Ås
21.03.2013 12:00	Partly cloudy/ Sunny after noon	21,4	21,9	110	825	598,6	22,5	27,6	24,5	23,7	-3,316	Not sun the whole hour
21.03.2013 13:00		21,6	22,2	92	894	766,1	22,7	29,2	25,4	24,9	-2,250	Not sun the whole hour
21.03.2013 14:00		22,0	22,0	75	911	860,3	22,0	29,4	25,7	23,4	-0,234	Not sun the whole hour
21.03.2013 15:00		21,9	22,1	115	839	865,9	22,3	29,6	25,7	26,2	1,701	
21.03.2013 16:00		21,7	21,8	147	764	809,5	22,0	28,9	25,3	25,5	0,926	
22.04.2013 10:00	Partly cloudy	22,1	22,1	187	454	532,4	22,0	27,3	24,7	24,0	-2,766	Not sun the whole hour
22.04.2013 11:00		22,3	22,4	182	537	537,4	22,5	27,8	25,1	26,7	6,175	Weather data from Ås
22.04.2013 12:00		22,5	22,7	174,8	707,2	538,4	22,9	28,3	25,4	24,9	-1,975	Not sun the whole hour
23.04.2013 11:00		22,8	23,2	121,8	822,4	389,8	21,6	27,4	25,1	25,1	-0,087	
23.04.2013 10:00	Partly cloudy	22,6	22,9	164	518	615,7	23,3	29,3	26,0	25,4	-2,037	Not sun the whole hour
23.04.2013 11:00		22,9	23,3	168	581	610,2	23,7	29,7	26,3	27,9	5,747	Weather data from Ås
23.04.2013 12:00		23,2	23,2	369	732	596,3	23,1	29,0	26,1	24,5	-6,448	Not sun the whole hour
23.04.2013 13:00		22,9	22,8	226,0	521	205,6	22,6	24,7	23,8	23,1	-9,077	Not sun the whole hour

$$rE = \frac{T_{opi} - T_{op,est,i}}{T_{opi}} \cdot 100 \%$$

# Thermal environment measurements and calculations



**Figure 11:** Comparison of measured operative temperature averaged over an hour and simulated operative temperature with IDA ICE 4.5.



**Figure 12:** Comparison of measured operative temperature and simulated operative temperature with IDA ICE 4.5 supplemented with calculated operative temperature in the sun with a time step of 5 min.

## Operative temperature in the sun measurements and calculations

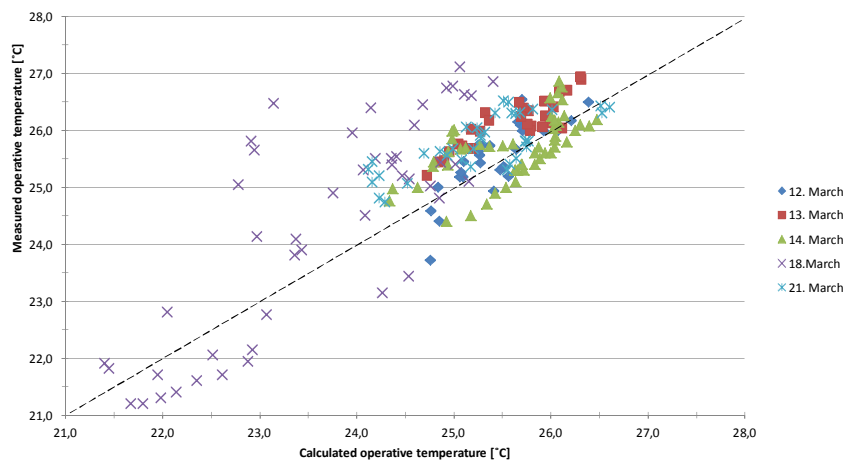


Figure 13: Scatter plot of measured predicted  $T_{op}$  against measured  $T_{op}$ . Measurement interval = 5 min. Observations  $n=200$ , correlation coefficient  $r=0,82$

## Uncertainty

- Uncertainty stem from
  - Use of climatic data of global solar radiation from Ås, 30 km outside Oslo
  - Modelling diffuse and direct radiation
  - Assumption of absorption of the globe thermometer
  - Measurement errors



## Summary & Preliminary conclusion

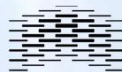
- Simulation tools for prediction of thermal comfort and energy use should implement assessment of how direct sun influence thermal comfort.
  - On-going process by Equa for IDA ICE 5
- The present validation indicate that the theory of Fanger work rather well for an object exposed to direct solar radiation.
  - Shorter time-step than 1 hour might be preferable.
  - Simplification: the sphere represent the human body
  - The “whole” body is irradiated
    - Future studies might have measurements in different heights
  - Simple calculation useful in the initial design of a building.

## Acknowledgement

- Silje Bjørkeng and Silje Navekvien (Master students HiOA spring 2013) for cooperation with conducting the measurements.
- Building owners of case study.

Thank you for your attention!

[Line-roseth.karlsen@hioa.no](mailto:Line-roseth.karlsen@hioa.no)



OSLO AND AKERSHUS  
UNIVERSITY COLLEGE  
OF APPLIED SCIENCES



AALBORG UNIVERSITY  
DENMARK